

Description of the Patent of Invention for
"Desalination Machine".

FIELD OF THE INVENTION

The present invention relates to a distillation process using vertical tube evaporators in a multi effect process and is applicable to desalination of sea water, brackish waters and in general to any water with dissolved solids, in order to produce fresh water for oil offshore platforms, ships, and for some arid locations, using rejected waste heat of thermal machines.

BACKGROUND OF THE INVENTION

Multi-effect distillation (MED) process has been used in industry for juice evaporation, to concentrate a substance, production of salts and for salty and marine water distillation for fresh water production.

In the MED process, only a portion of the concentrate submitted to the heat transfer surfaces is evaporated. Each effect works in a different pressure. The remaining liquid of each effect, normally called brine, is fed to the liquid tray of the next effect or stage, where part of it flashes into vapour. Produced vapour in one effect will give up heat to boil the liquid transferred to the next effect due to the temperature difference between them.

Normally the effects or stages have evaporators located in separate chambers, requiring a pipeline for conducting vapour from one stage to the next, as shown in the US Patent numbers 3884767, 3261766 e 3021265.

SUMMARY

Intended to improve the performance and reduce the dimensions of this kind of equipment, the present invention

is developed assembling the several evaporators in a concentric disposition, using a shell and tube exchanger for the first stage and a bundle of tubes for the succeeding stages, which are inserted one inside each other. Through
5 this constructive arrangement, the following advantages are achieved: material reduction due to the absence of vapour pipelines; vapour friction losses reduced to a minimum; smaller size due to the compactness of the concentric disposition of evaporators; no heat loss in the inner stages;
10 cost effectiveness.

This unit can also be used to concentrate a mixture, using low temperature evaporative process.

Fresh water makers are extensively used in oil offshore platforms and ships, normally using the heat of
15 exhausted gases of thermal machines.

The figures attached, are representative of four different models, showing their respective stages, all using the same constructive arrangement, here named concentric evaporators. The higher the number of stages the lower the
20 energy consumption per volume produced. The choice for the number of stages, depend on the available heat, the fresh water rate desired and of course the involved costs.

The unit can be designed to produce any desired flow rate, meanwhile it is usual for this kind of equipment
25 to have a production flow rate ranging from 5 until 120 m³/d.

The dimensions of a 60m³/d desalinator have approximately 2.2 m height and 1.2 m in diameter.

DESCRIPTION OF THE DRAWINGS

The different models will now be exemplified with reference to the accompanying drawings briefly described hereafter.

Figures 1 to 9 are representative of the two stage
5 model.

Figure 1 is the elevation view in cross section of the two stage model totally assembled;

Figure 2 is the top view of the first stage evaporator here named Ring Shell and Tube Evaporator;

10 Figure 3 is the elevation view in cross section of the Ring Shell and Tube Evaporator;

Figure 4 is the top view of the second stage evaporator, here named Cylindrical Bundle Evaporator, that is the ultimate stage;

15 Figure 5 is the elevation view in cross section of the Cylindrical Bundle Evaporator;

Figure 6 is the bottom view of the floating head of the Cylindrical Bundle Evaporator;

20 Figure 7 is the top view of the condenser inserted into the superior chamber;

Figure 8 is the elevation view in cross section of the condenser;

Figure 9 is the condenser front view;

25 Figures 10 to 15 are representative of the three stage model;

Figure 10 is the elevation view in cross section of the three stage model totally assembled;

30 Figure 11 is the elevation view in cross section of the first stage of the three stage model, or the Ring Shell and Tube Evaporator;

Figure 12 is the base support for intermediate stage, where A is the top view and B is a cross section view;

Figure 13 is the elevation view in cross section of the intermediate stage, here named Ring Bundle Evaporator;

5 Figure 14 is the bottom view of the floating head of the Ring Bundle Evaporator;

Figure 15 is the cross section of figure 14;

Figure 16 is the elevation view in cross section of the four stage model.

10 DETAILED DESCRIPTION OF THE INVENTION

The following description is referred to figures 1 to 9, all related to the two stage model, whose operational philosophy is extensive to the other models.

15 Figure 1 shows the two stage model with its evaporators assembled in the concentric arrangement where is observed that the second stage (Fig. 5) is assembled inside the first stage (Fig. 3), supported and bolted at the flange 1 (Fig 3). A gasket is used to avoid leakage. The upper chamber (Fig. 7) with the condenser 2 inserted into it, is 20 assembled bolted in the same flange 1.

On figures 2 and 3, is observed that the first stage is constituted of a shell and tube exchanger without part of the central tubes, here called Ring Shell and Tube Evaporator. The inner wall 3 encloses the hot water 25 throughout the interior of the shell, returning for heating on outlet 5.

Salt water feeds the first stage on nozzle 6, passing throughout the chamber 7, and directs to the first stage tubes 8, receiving enough heat from hot water 4, until 30 boiling. Heat is furnished so that only part of the water is

vaporised in order to avoid excessive scales into the tubes. It is observed on figure 2 that the vapour chamber above the evaporator is enlarged in order to permit the passage of the vapour to the condensation chamber 9 (Fig 3).

5 Hot water temperature 4 is heated at maximum 88 °C in order to avoid excessive scales into the tubes. Operating evaporative temperature ranges from 60 to 65 °C on the first stage and from 45 to 50 °C on the second. To obtain these evaporating temperatures, the pressure must be evacuated and
10 controlled in the range of 20,0 to 25,0 kpa abs at the first stage and in the range of 9,9 to 12,4 kpa abs at the second stage. Vacuum is obtained by an eductor 10 (Fig. 1) that sucks the non condensable gases like air and carbon dioxide through the first stage vacuum outlet 11, and second stage
15 vacuum outlet 12. Salt water at a specific designed pressure 13 (Fig. 1) is used to drive the eductor.

Boiling water and vapour rises into the tubes 8, splashing on the plate 14 (Fig. 3). Vapour flows to the second stage evaporator tubes 15 (Fig 1 and 5), here named
20 Cylindrical Bundle Evaporator. Touching the tube walls, the vapour condenses, giving up energy to boil the second stage salt water. The condensate produced is collected on the bottom of the chamber 9 (Fig. 3) and pumped to a storage tank through the outlet 16, delivering sensible heat to the
25 incoming salt water 6 through the bundle 17, inside chamber 7.

Second stage is fed by the remaining not vaporised first stage salt water, suctioned by the second stage lower pressure through tube 18, pouring into the tray 19, and
30 flashing vapour. Tube 18 collects salt water from the bottom

of an extended pipe, in order to keep an adequate water column, to avoid suction of vapour from the first stage. On the tray, water directs to the central tube 20, dropping to floating head 21, feeding second stage tube bundle 15. Tray 5 19 and plate 14 prevent rising salt water droplets to reach the demisters 22 (first stage) and 23 (second stage). Both plate 14 as tray 19 are removable in order to permit access to the tube sheets.

Second stage fresh water is obtained through the 10 vapour condensation on condenser 2, being collected in the container 24. Through outlet nozzle 25 (Fig.1), condensate is pumped to reservoir. Inside condenser tubes circulates cold salt water through inlet nozzle 26 (Fig. 1), leaving on nozzle outlet 27. Here, stream 4 is derived in order to feed 15 first stage. Returned salt water 28 is discharged.

Level is maintained on the first stage by the weir 29. In the same way, second stage level is maintained by weir 30. Salt water that overboards weir 30 exits the unit through outlet 31, being suctioned by eductor 10 (Fig 1) to discharge 20 32 (Fig.1).

Nominal flow rate is obtained through control valve 33 and flow meter 34 (Fig.1). Instruments as thermometers and manometers are used for operational control, and a pressure safety relief valve 35 installed on the first stage grants 25 against over pressure.

A thin steel shell 36 (Fig. 5), here named armour, which is assembled in two halves by flanges, encloses second stage tube bundle. The role of this armour is to direct the vapour to pass through the tubes, avoiding being .suctioned 30 directly to vacuum pipe 11 (Fig. 1). The welded edge 37 (Fig.

5) supports the armour at the top of the first stage inner shell 3. A gasket bonded bellow the edge avoids vapour leakage.

A cut 38 (Fig. 6) made at the bottom tube sheet and 5 at the floating head 21, permits the passage of the fixed vacuum pipe 11.

The following description is referred to Figures 10 to 16 of the three stage model.

Three stages model (Fig. 10) has the same two stage 10 constructive philosophy, with a new intermediate stage included, here named Ring Evaporator Bundle (Fig. 13), that becomes the second stage, and is inserted into the first stage. The cylindrical evaporator (Fig. 5), becomes now the third stage, and is inserted into the Ring Evaporator Bundle 15 (Fig. 13).

The first stage of this model (Fig. 11) is similar to the two stage model, but the base 39 (Fig. 11) is now welded to the inner and outer shells 40 and 41 respectively (Fig. 11), in order to have a reliable watertight. At the 20 centre of this base is welded a support 42 (Fig. 11 and 12), in order to hold and centralise the intermediate stage (Fig. 13).

On this model, vacuum lines 43 and 44 (Fig. 11) and distillate outlets 45 and 46, are located bellow the unit, in 25 order to permit easy access of second and third stages.

Heat exchange is accomplished through a 15 to 20 °C differential temperature between stages.

Ring Evaporator Bundle has also an armour 47 (Fig. 13), in order to direct the first stage vapour to its bundle 30 48. Floating head 49 has in this way a ring format also, as

shown on figure 14 (bottom view) and figure 15 (section view). An internal shell (50) encloses and isolate the vapour inside this stage.

The material used in the unit needs to be corrosive
5 resistant to salt water as aluminium bronze, monel, copper
nickel, and titanium.

Four stages model is represented in a section view
on figure 16. Now, another Ring Evaporator Bundle is
included, as an intermediate stage, compounding in this way
10 the four stage model, and so on.